



Installation of Jasmund jacket - theory and practice

Introduction presenters



Lars van Heugten

Marine engineer, HMC

Msc Marine Technology – working on ship hydrodynamics and stability as well as operational support



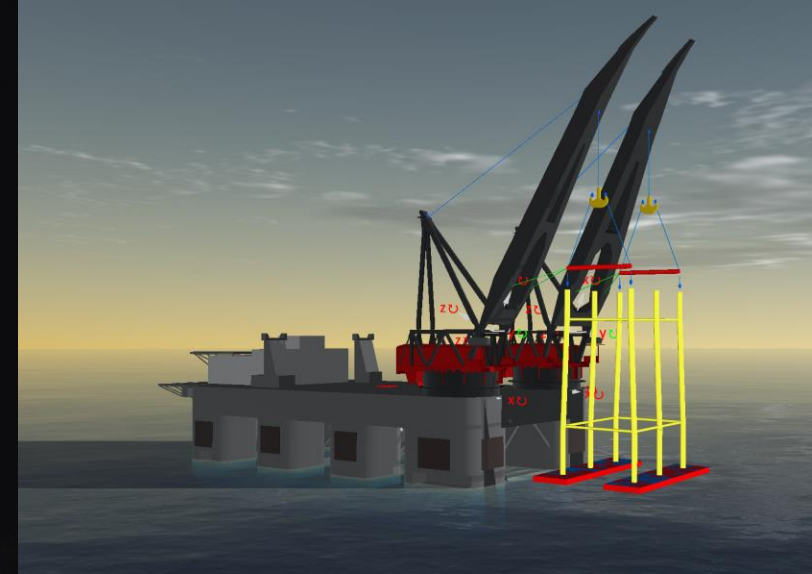
Henrik Schrader Bordal

Analysis engineer, Entail

MSc Marine Hydrodynamics – working with marine operation analysis and software development

Agenda

- Project introduction
- Unique challenge
- How to solve the challenge
- Operational insights

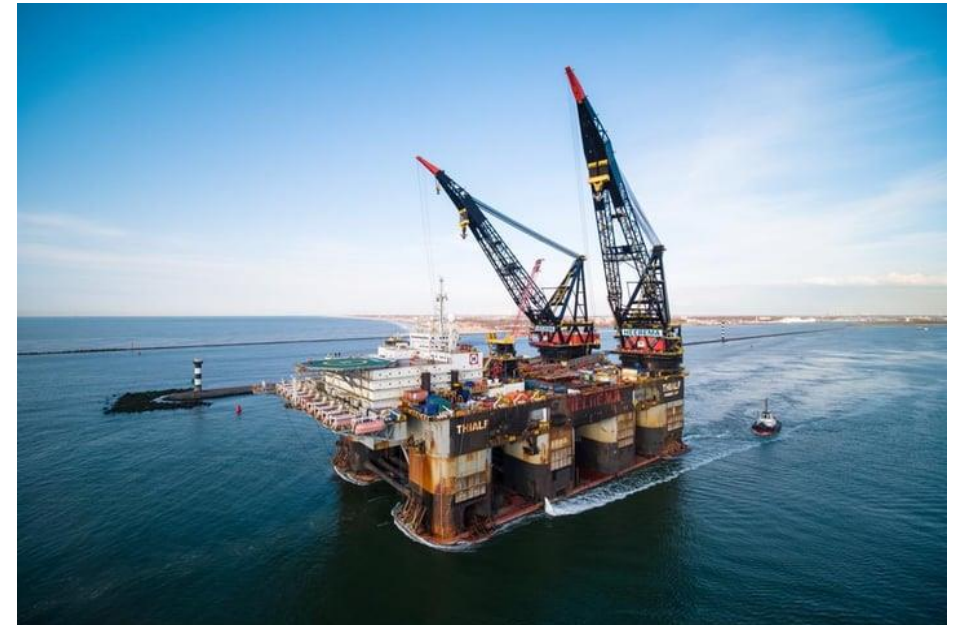


Project introduction: Jasmund OSS

- Project:
 - Substation capacity: 300MW
 - Components: 4400mT jacket
5300mT topside
 - Location: Baltic Sea

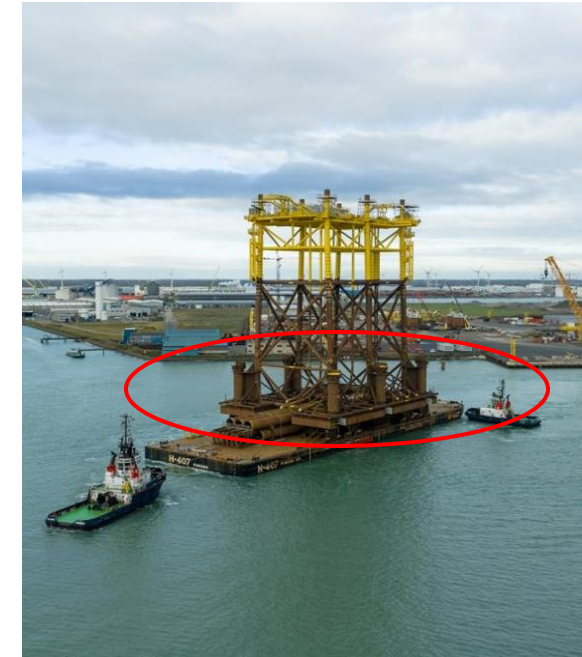
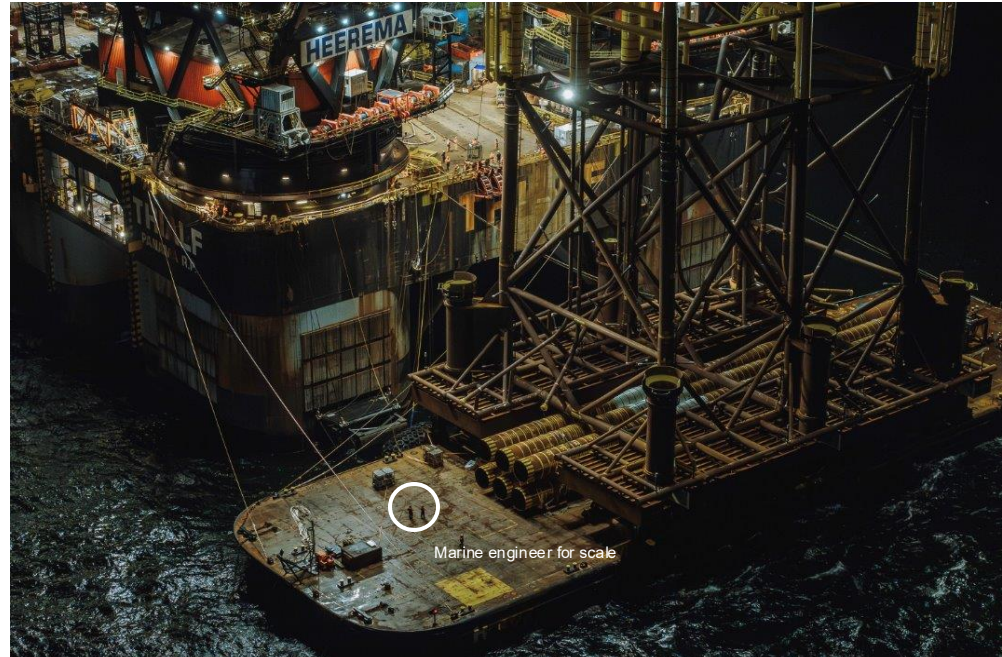


- Installation vessel Thialf
 - Lift capacity: 14,200mT
 - Length: 202m
 - Width: 88.4m

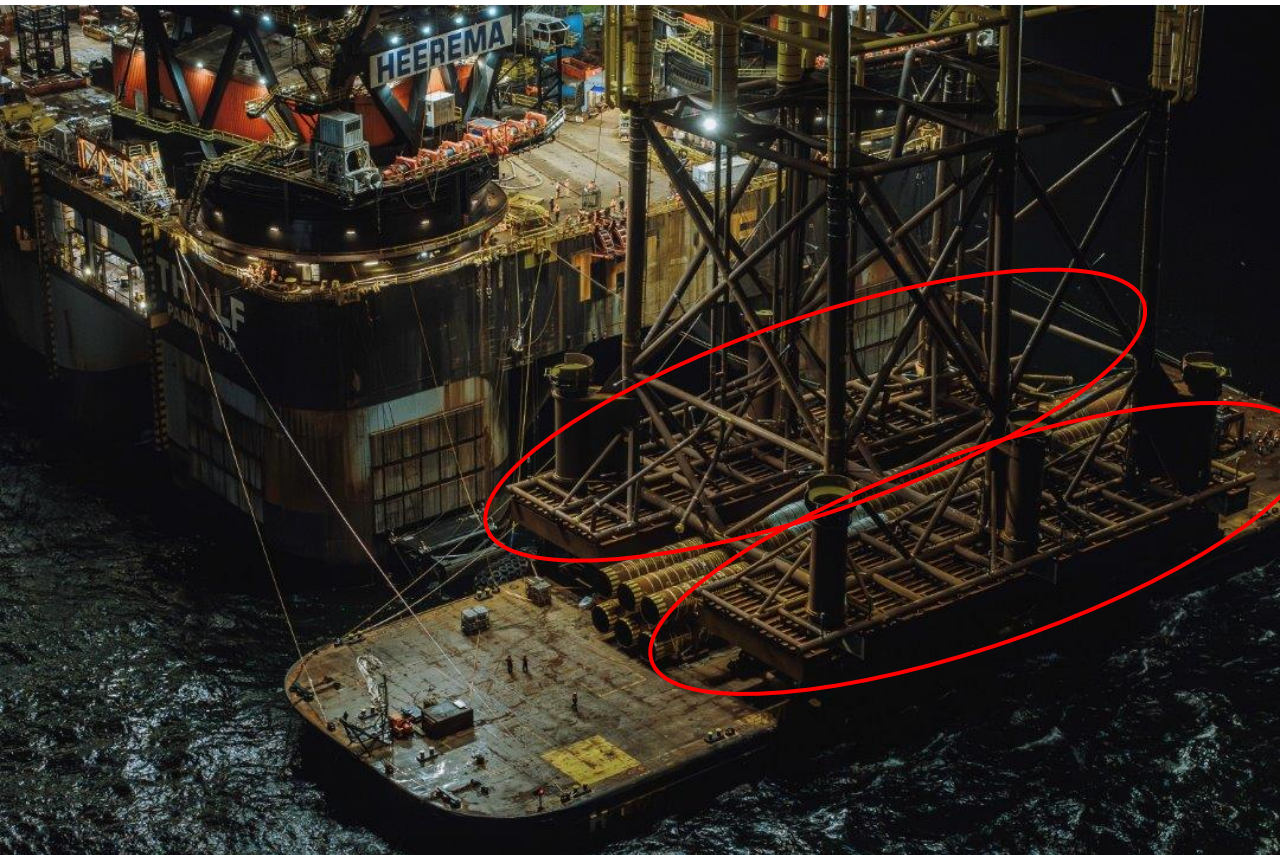


Typical marine scope jacket installation as installation contractor

- Transport
 - Stability
 - Accelerations
 - Barge strength
 - Bollard pull
- Mooring and Lift analysis
 - System dynamics
 - Operational limits
- Offshore Decision Support
 - Winter campaign

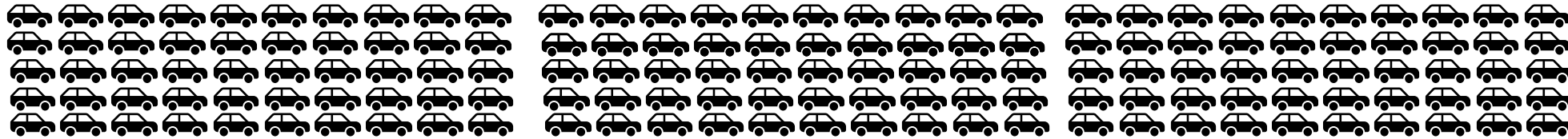


Unique challenges

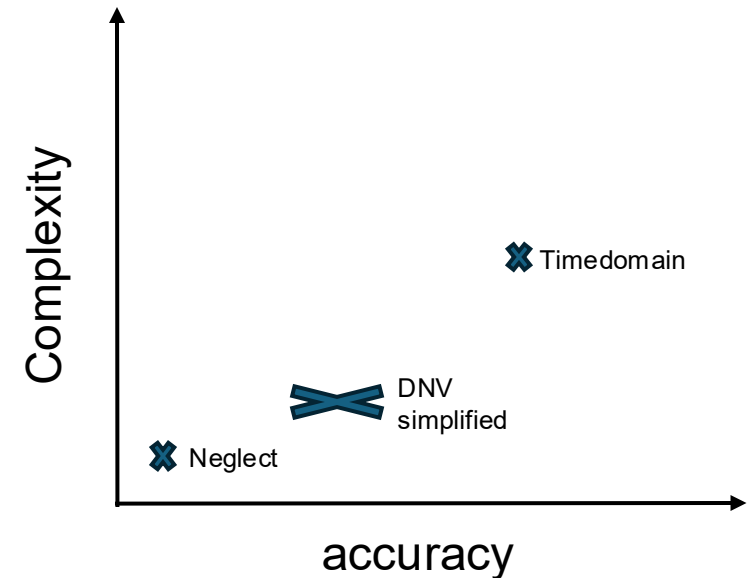


Unique challenges

- Large mudmats can cause large dynamics (or even snap loads) in rigging



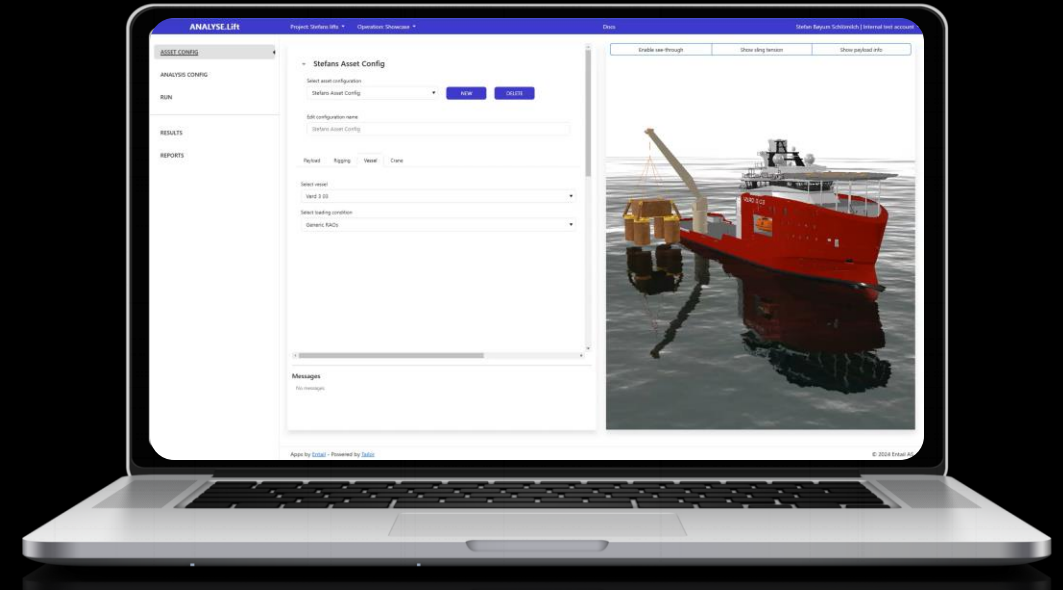
- How should we deal with large slamming areas while lowering through the waterline
 - Neglect effects?
 - DNV-RP-N103: Lifting through the waterline?
 - Different options?
- DNV:
 - Lowering velocity + Cranetip dynamics + orbital wave velocity = total impact velocity
 - Slamming area = total slamming surface (projected area to the wave)
 - DNV: *"The horizontal extend of the lifted object is relatively small compared to the wave length"*
 - Result:
 - Zero workability
 - $H_s < 0.5m$



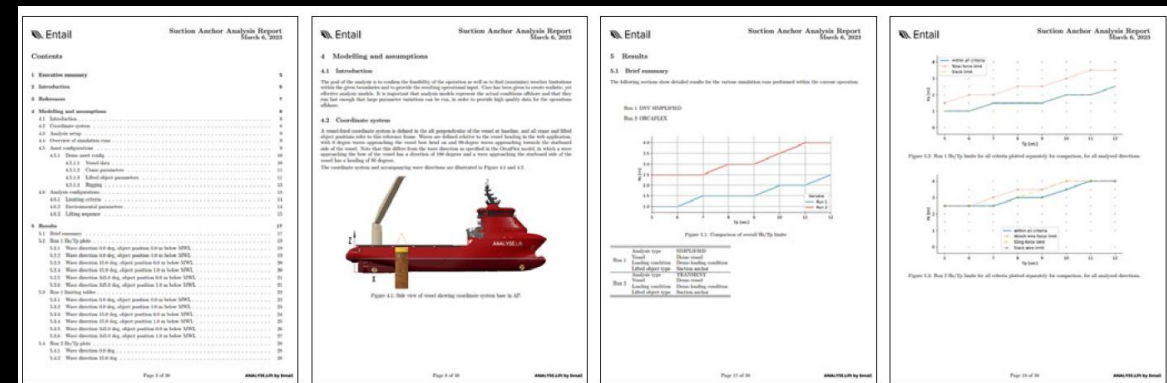
ANALYSE.Lift

Quick iterations through efficient engineering

- Built on 10 years of automation experience in 100s of projects
- Completely integrated workflow
- All these manual tasks have been automated:
 - Model building
 - Assigning hydrodynamic parameters
 - Creation of batch files
 - All file handling
 - Running of files
 - Post processing
 - Report writing

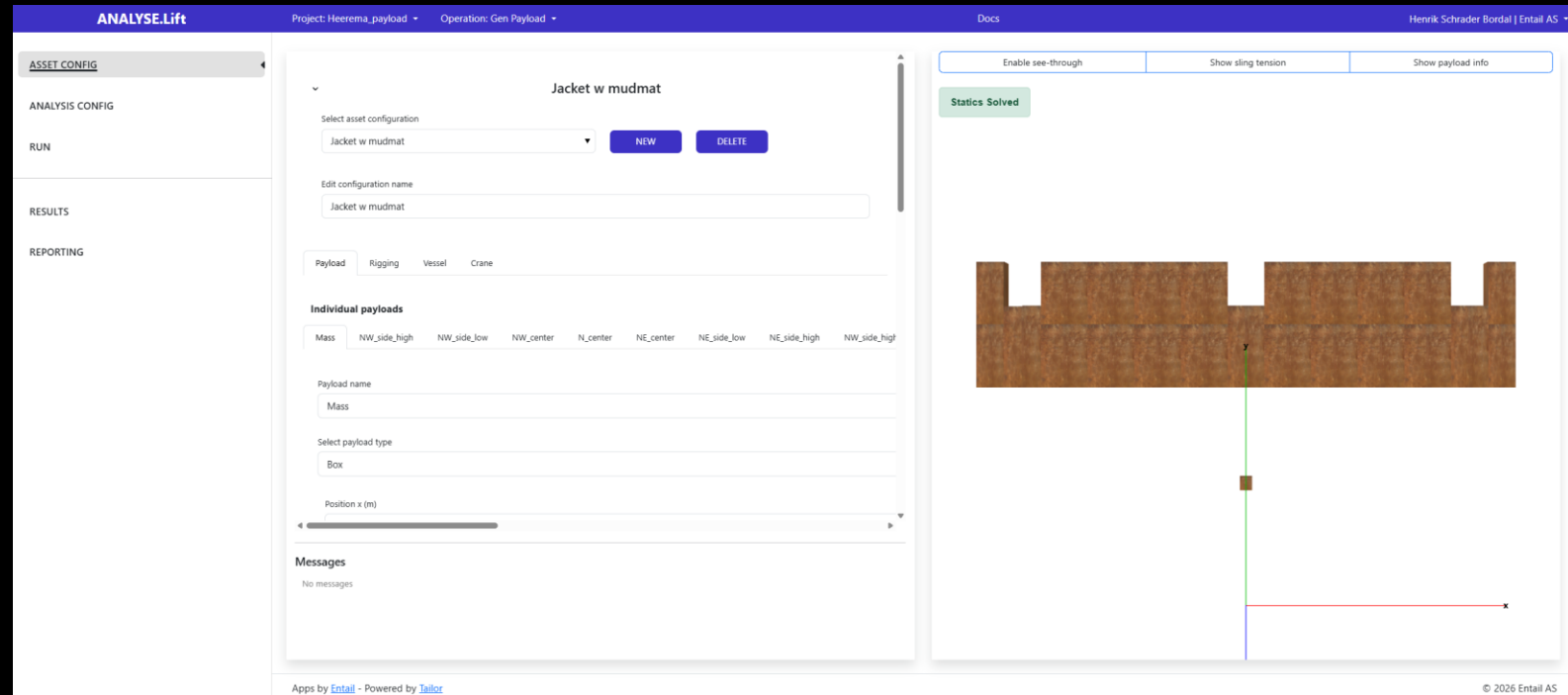


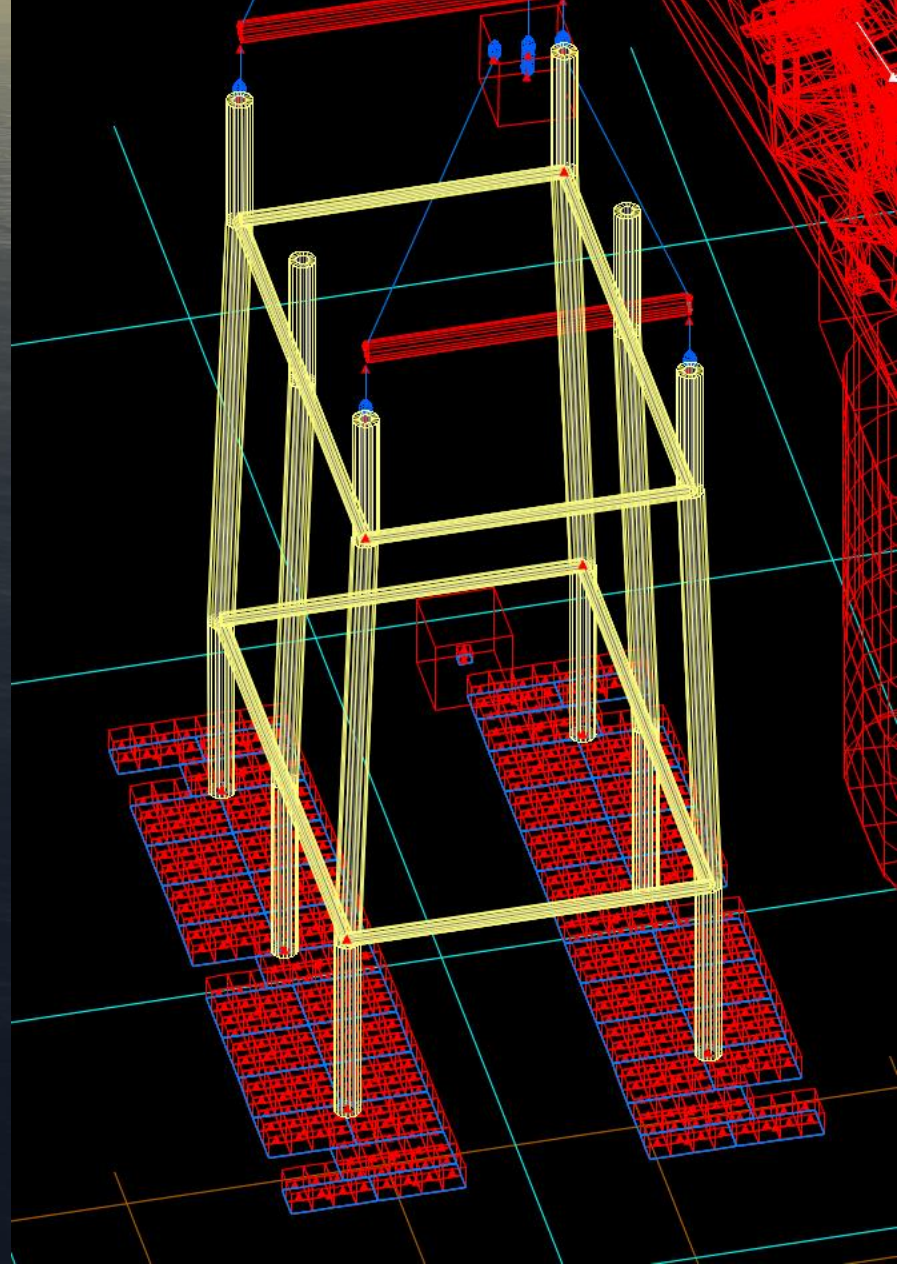
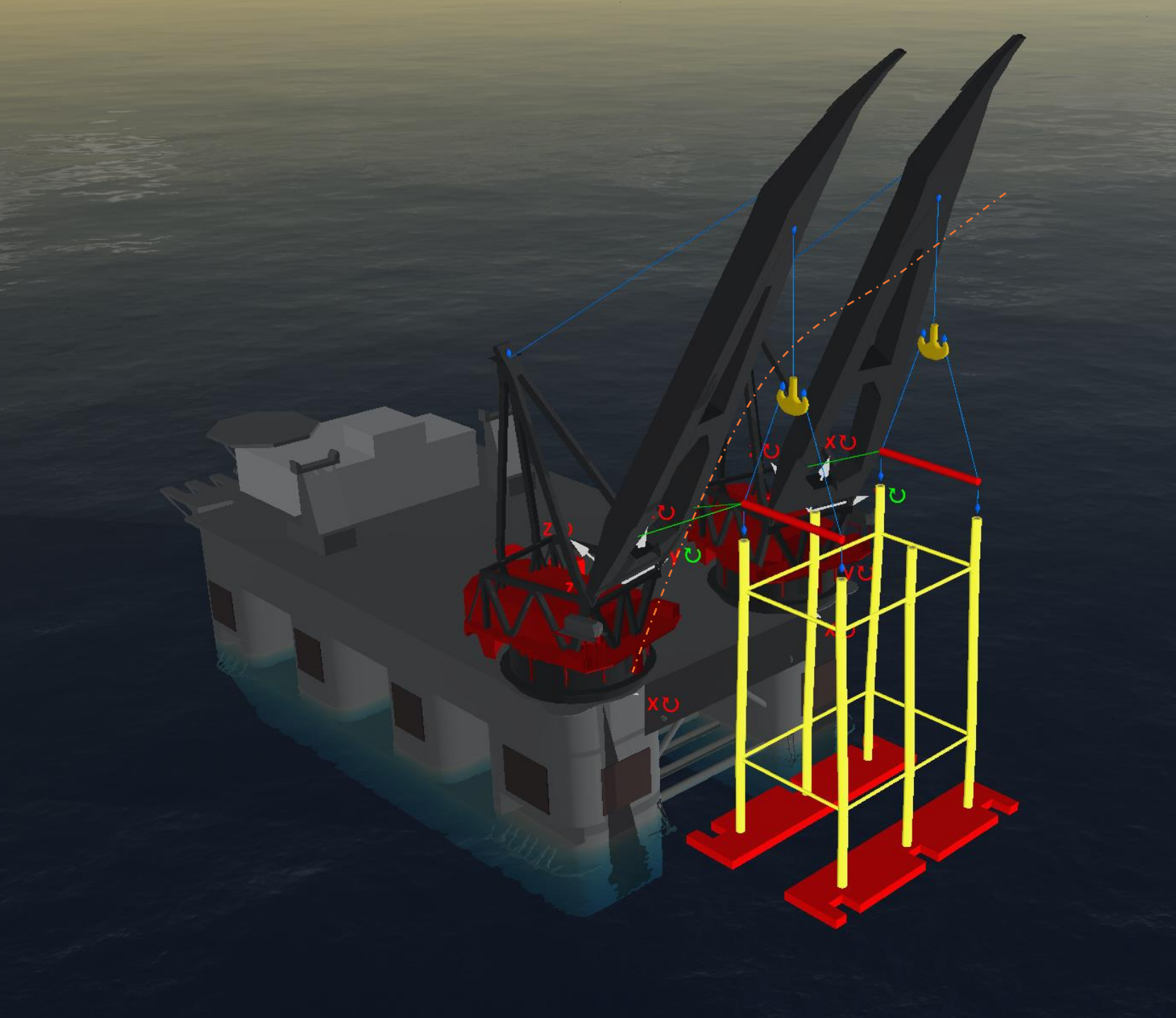
30 min



ANALYSE.Lift

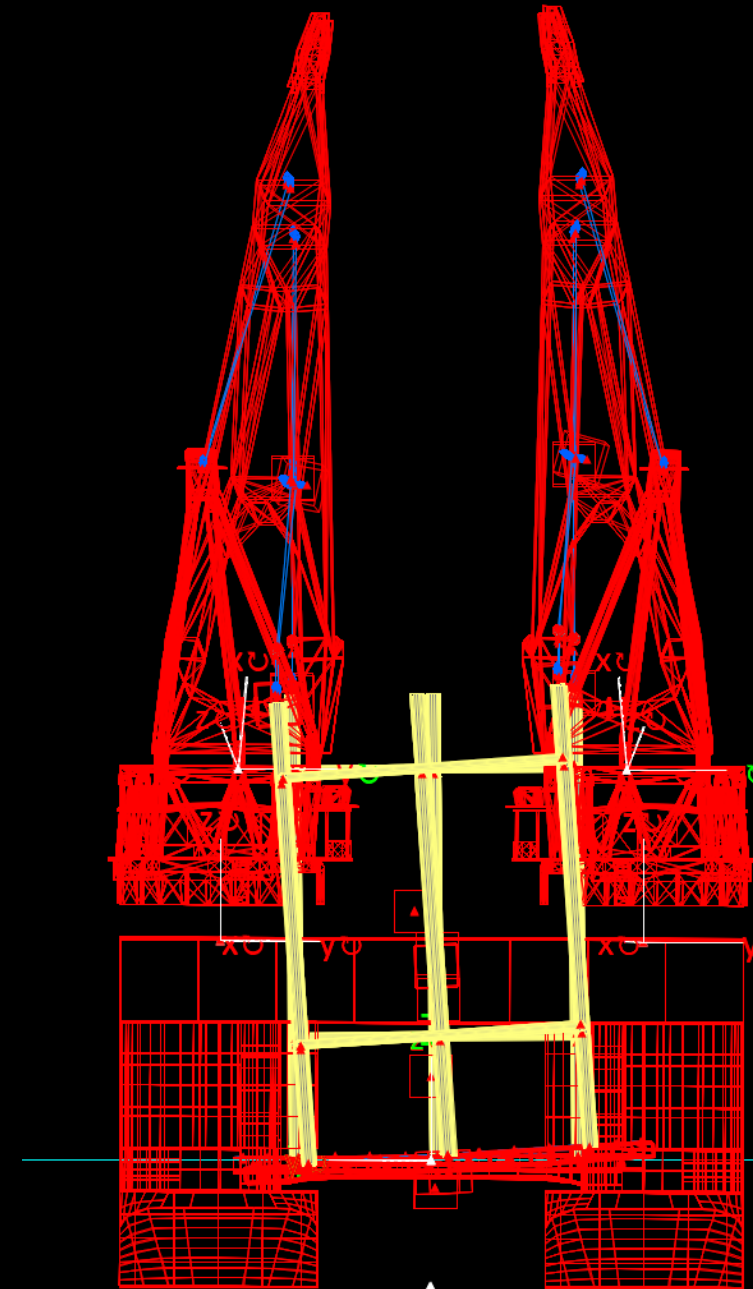
- Used Entails software ANALYSE.Lift to model mudmats and jacket mass properties
- Automatically models as OrcaFlex 6D Buoys -> using Morisons equation for hydrodynamic loads
- Allowed us to do ~30 iterations with 21000 analyses per iteration





Eigenmode analysis

- Two crucial eigenmodes identified
 - Jacket roll ($\sim 7s$)
 - Jacket pitch ($\sim 3s$)



Analysis

- Strict weather criteria -> need to refine model
- Alternatives
 - Transient analysis
 - Tilted lift
 - Tugger lines
 - Include shielding effects (free heading)
 - Wave spreading
 - Diffraction analysis

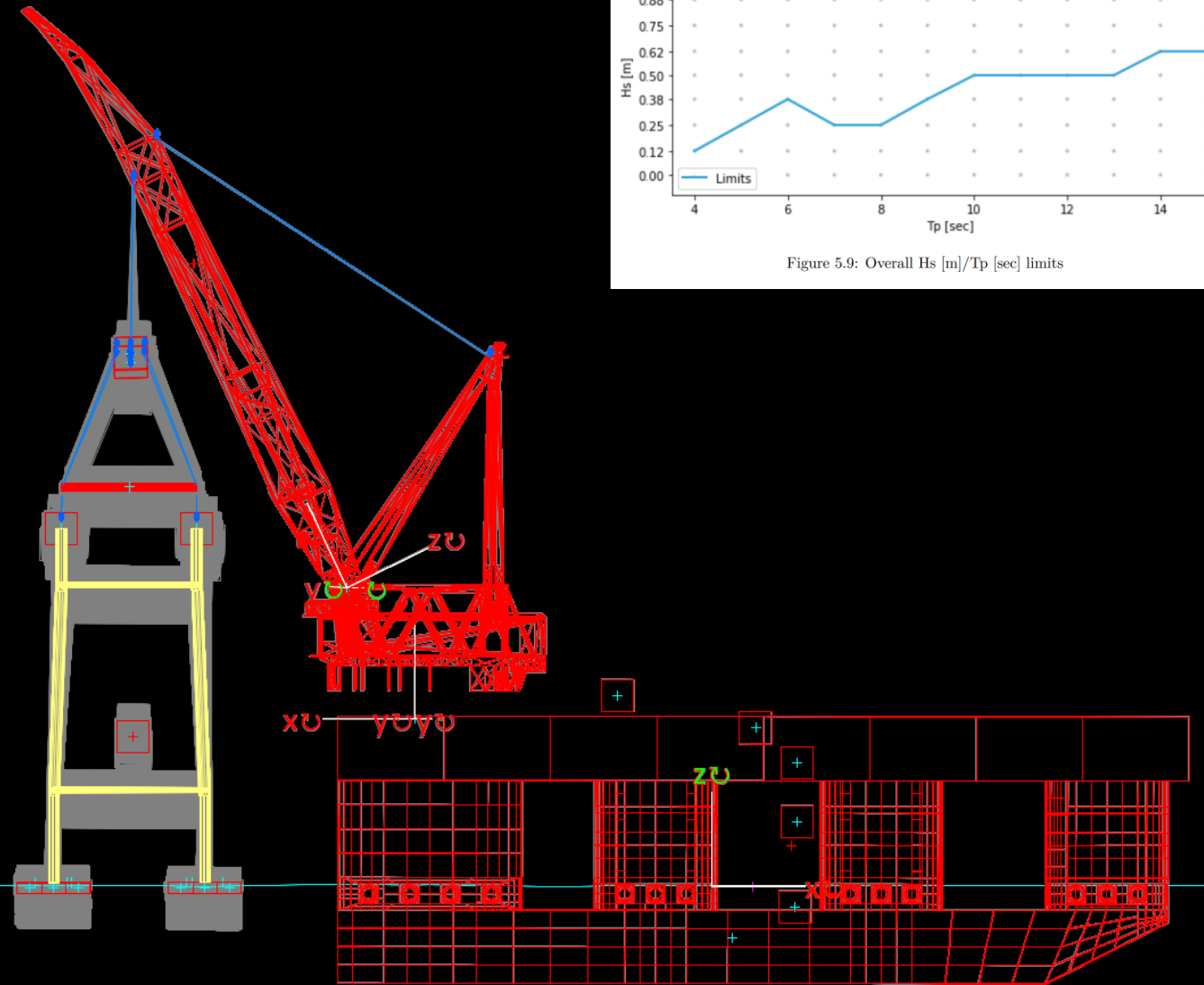
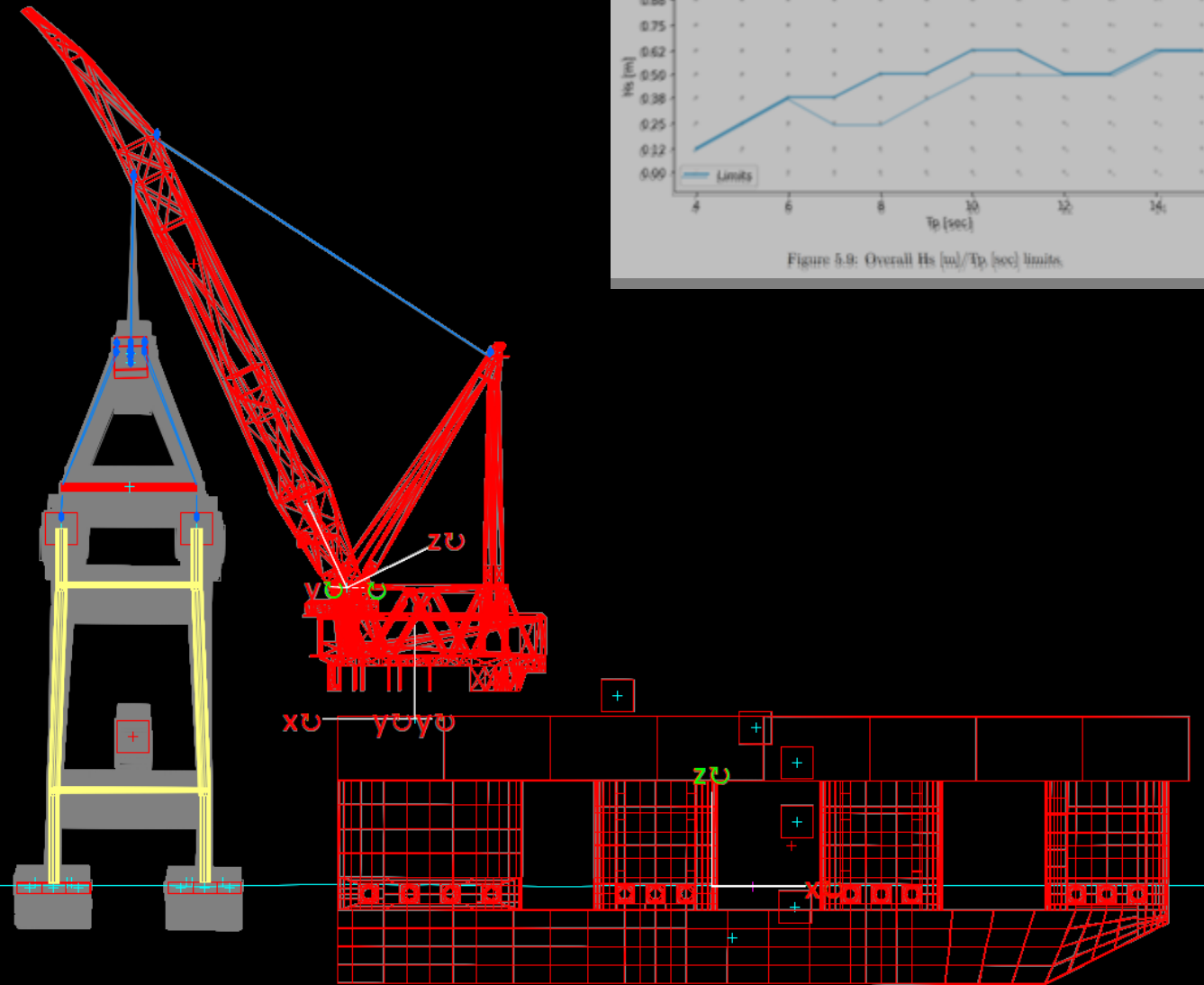


Figure 5.9: Overall Hs [m]/Tp [sec] limits

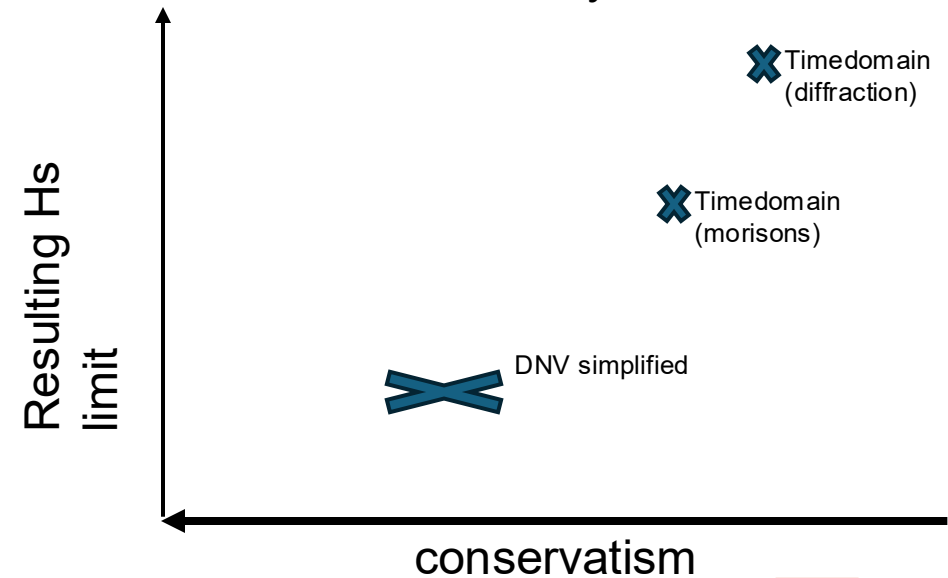
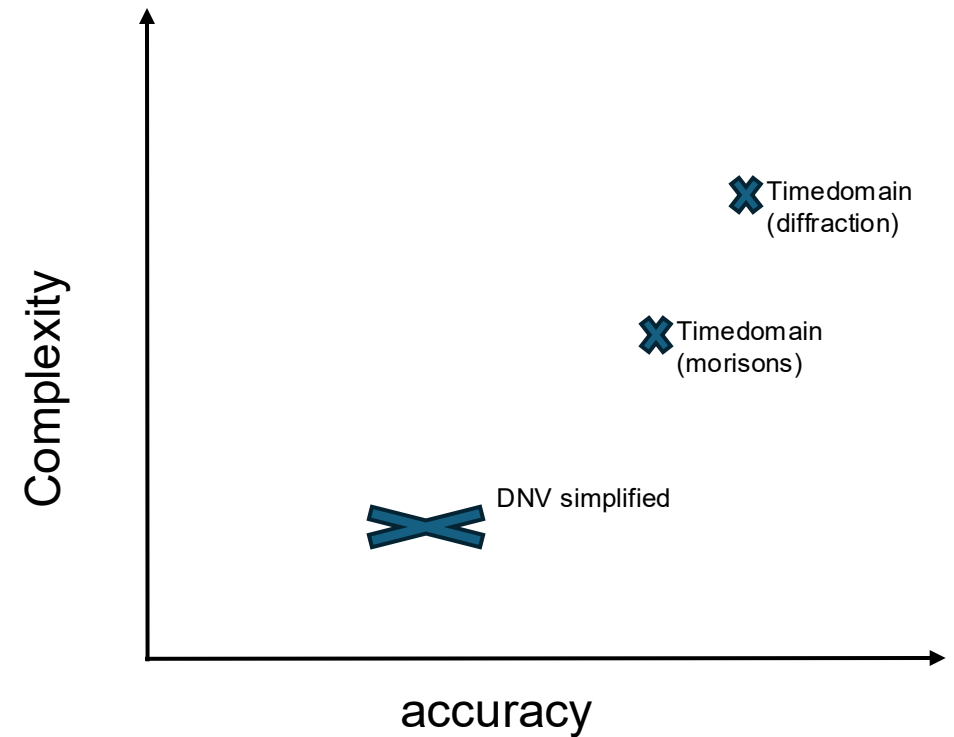
Analysis

- Strict weather criteria -> need to refine model
- Alternatives
 - **Transient analysis**
 - **Tilted lift**
 - **Tugger lines**
 - Include shielding effects (free heading)
 - **Wave spreading**
 - **Diffraction analysis**



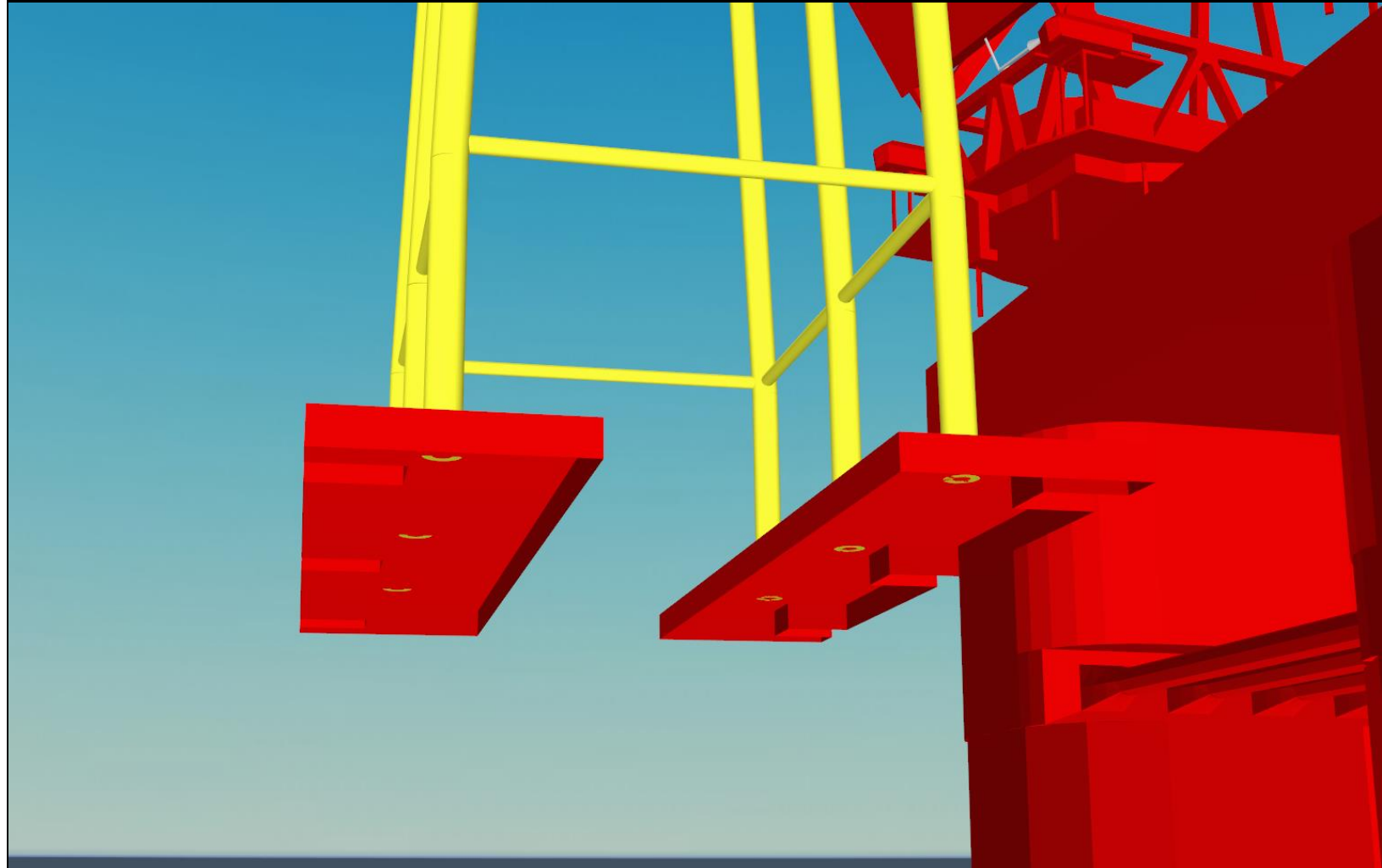
Comparison of methodologies

- Morisons
 - Assumes small objects
 - Object does not disturb the wave
- Diffraction
 - Object disturbs wave
 - Includes effect of 'altered wave' and radiation due to object motion



Diffraction analysis

- Modelling mudmats and creating mesh
- OrcaWave diffraction analysis at several waterdepths
 - Balancing mesh size, submergence and computational cost
- Vessel object represents the frequency-dependent added mass, damping and excitation forces
- 6D buoys represent drag and slam forces



Diffraction analysis




- Modelling creating
- OrcaWay analysis waterdep
 - Balance subm comp
- Vessel of the frequ added m excitation
- 6D buoys represent drag and slam forces

✓ Final-Final Nuclear-Plus Option:

We must:

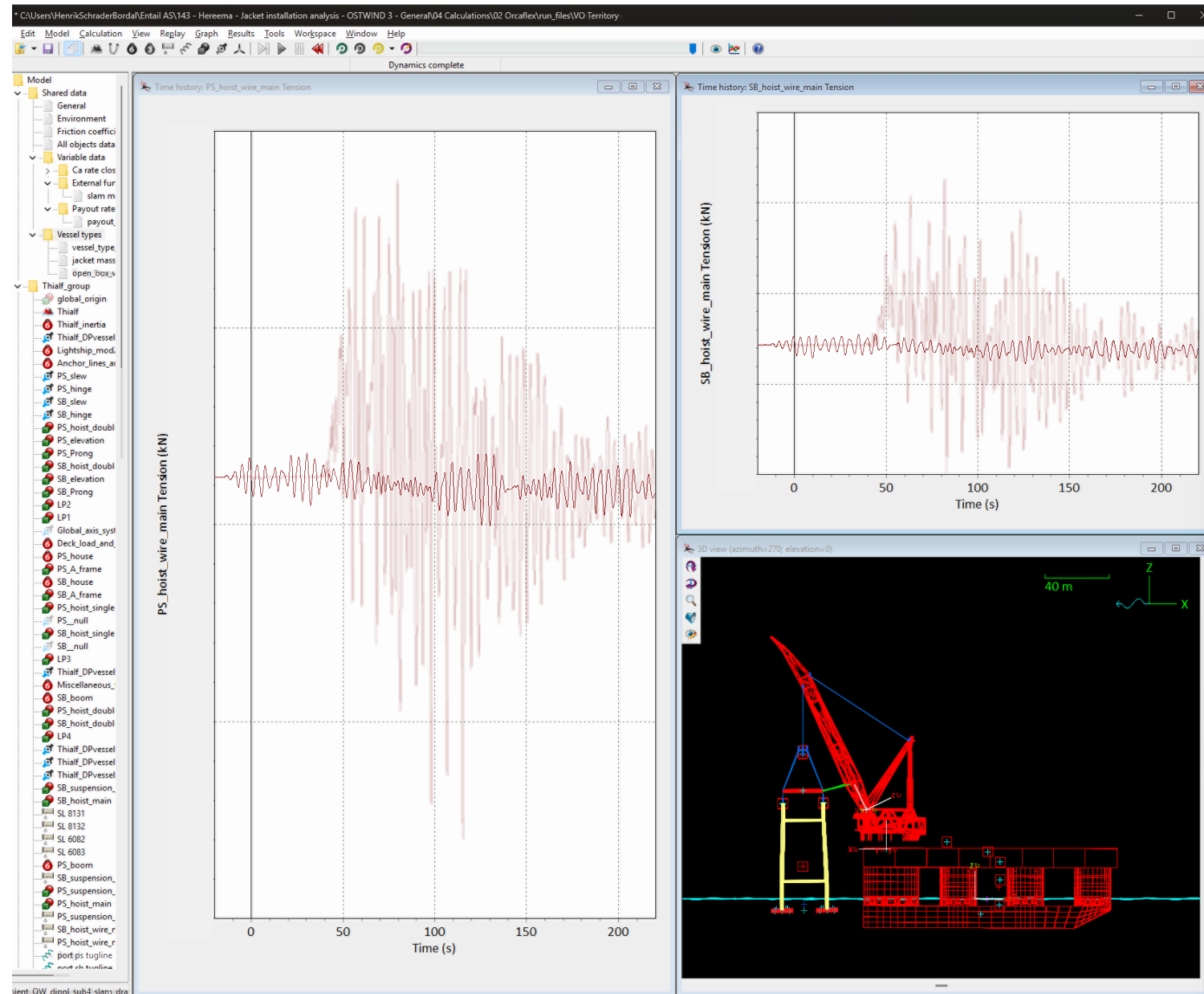
1. Rebuild the mesh from scratch
2. Identify the exact **shared vertex** above
3. Create a **bridging triangle** or **reindex faces** to force both shells to use the same vertex instance

Would you like me to:

-  Rebuild the mesh right now using shared face indexing across that point?
-  Just output a list of all shared coordinates between the shells so you can stitch them in Rhino?
-  Call it a day and start drinking?

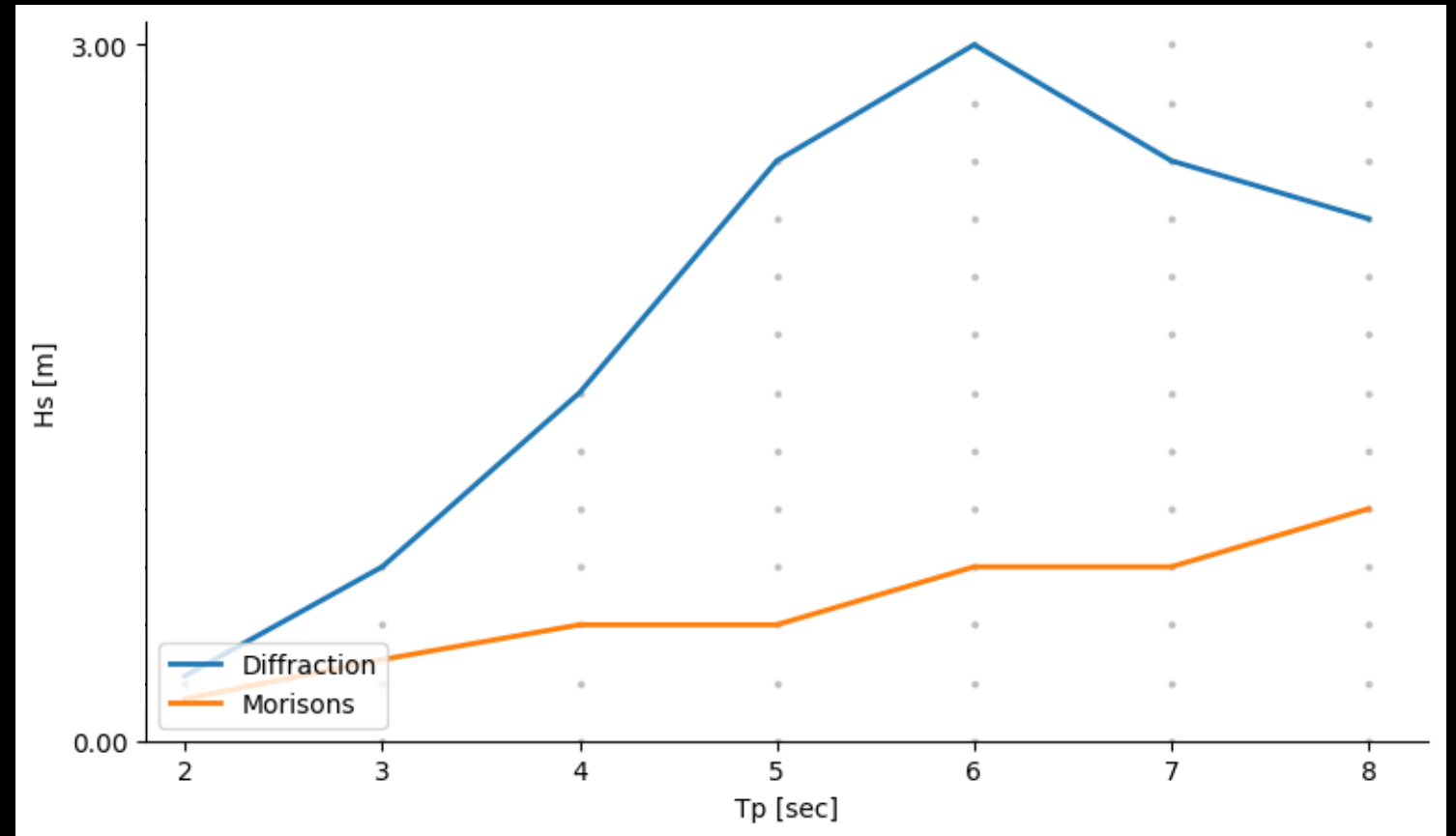
Your call, commander. [->]

Comparison of time series:

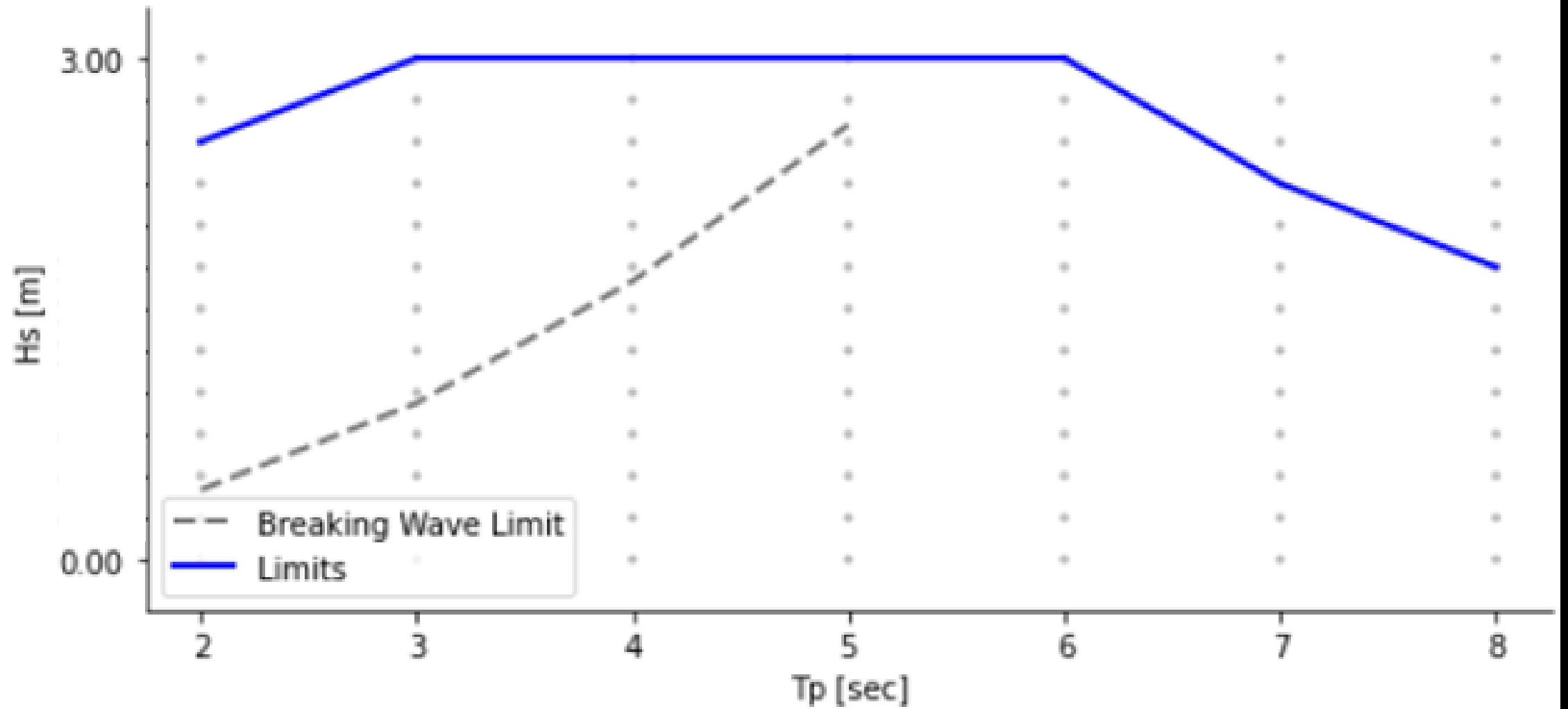


Results

- Omnidirectional results presented to the right
- Analysis limited upwards by wave steepness criterion given in DNV



Results

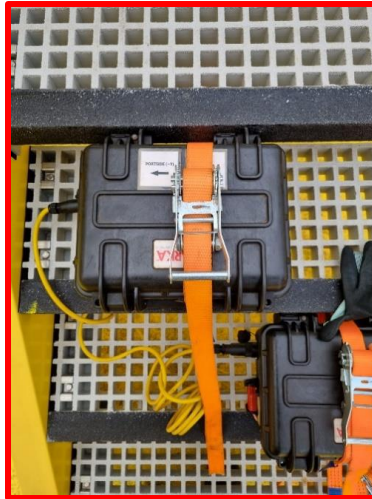


Model validation and learning from offshore



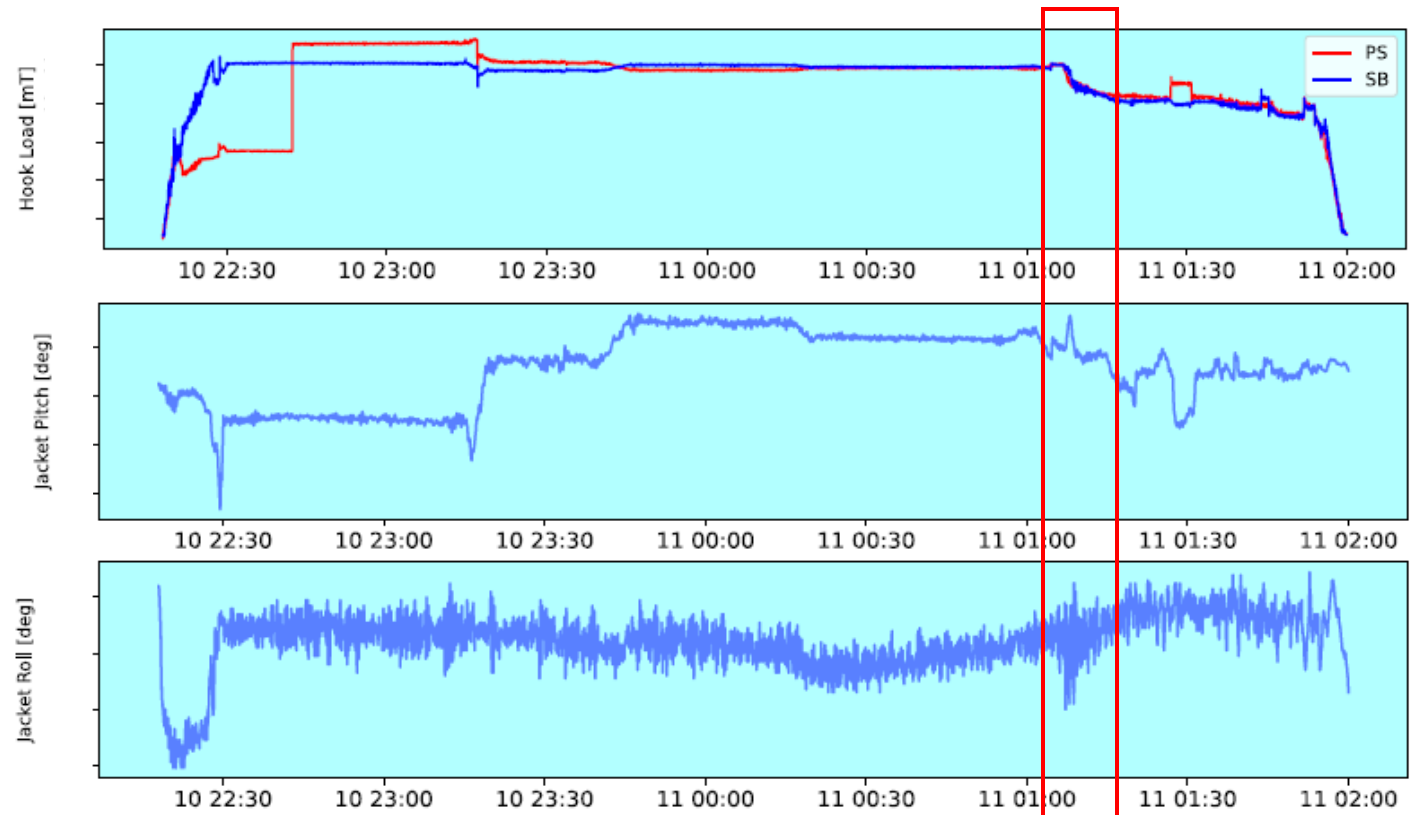
How to 'validate' a model

- Gaining insight by:
 - Vessel sensor data: Hoist wire loads
 - Tarka box motion sensors
 - Wave rider buoy



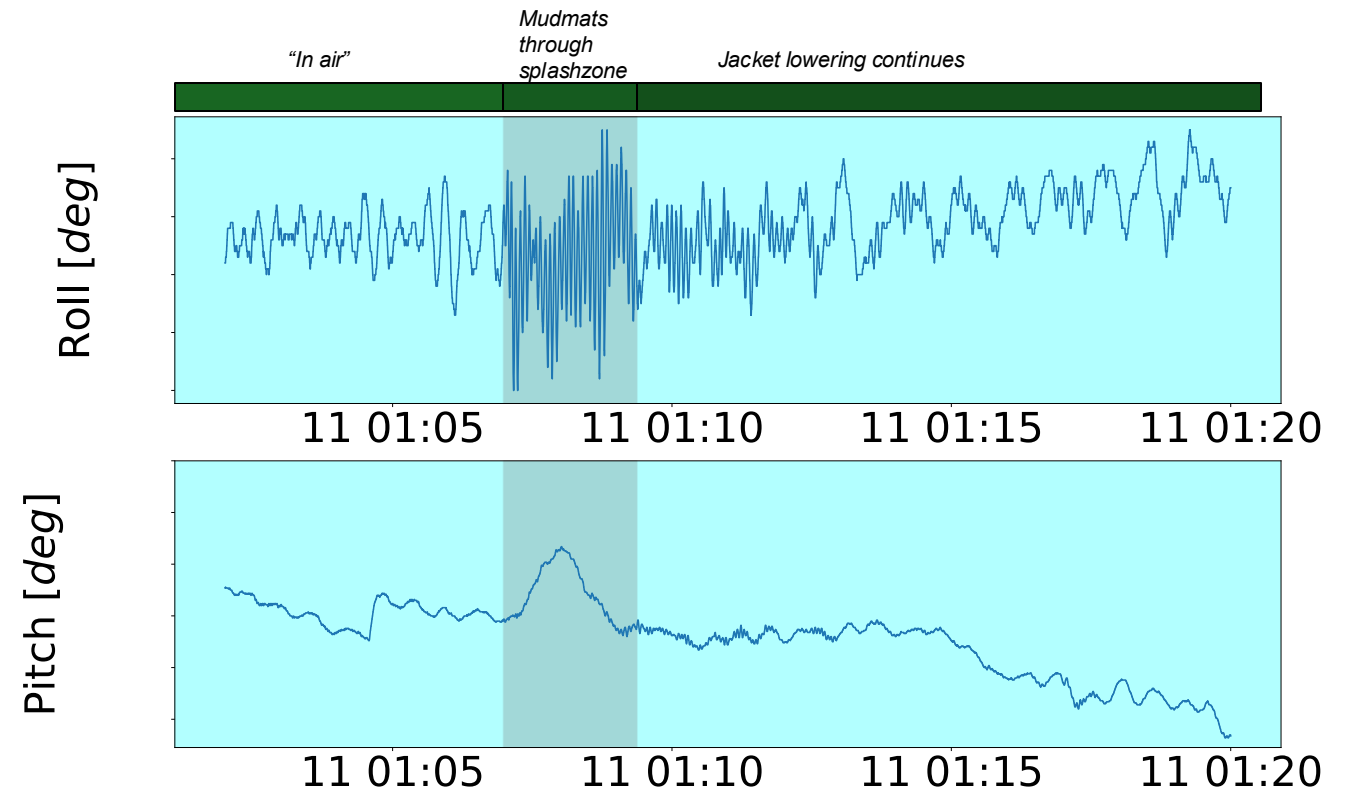
Timetraces total installation

- Benign conditions
($H_s \sim 1.0-1.5$ m, $T_p \sim 5$ s)
- Very small increase in DAF
- Small peak in jacket pitch
- Significant increase in jacket roll



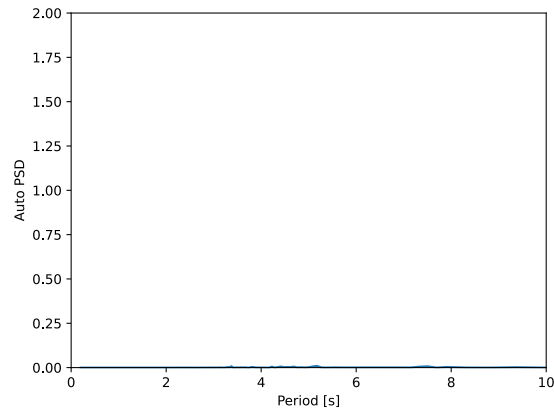
Splashzone Tarka data

- Jacket roll increased in splashzone
- Trim was increased to lower slamming loads
- Different period compared to other stages



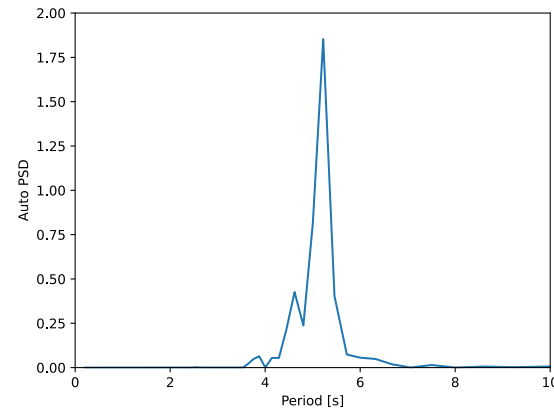
Splashzone spectral data – jacket roll

"In air"

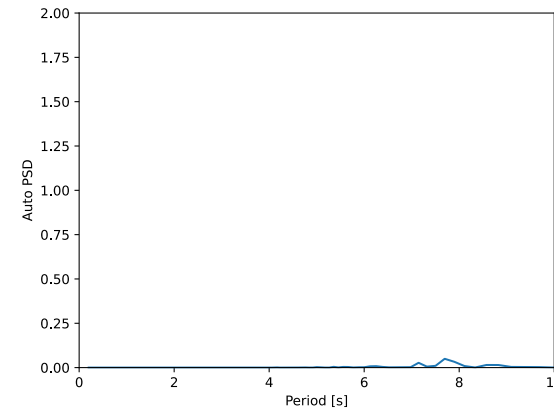


*Power at higher periods
> 10 s*

*Mudmats
through
splashzone*



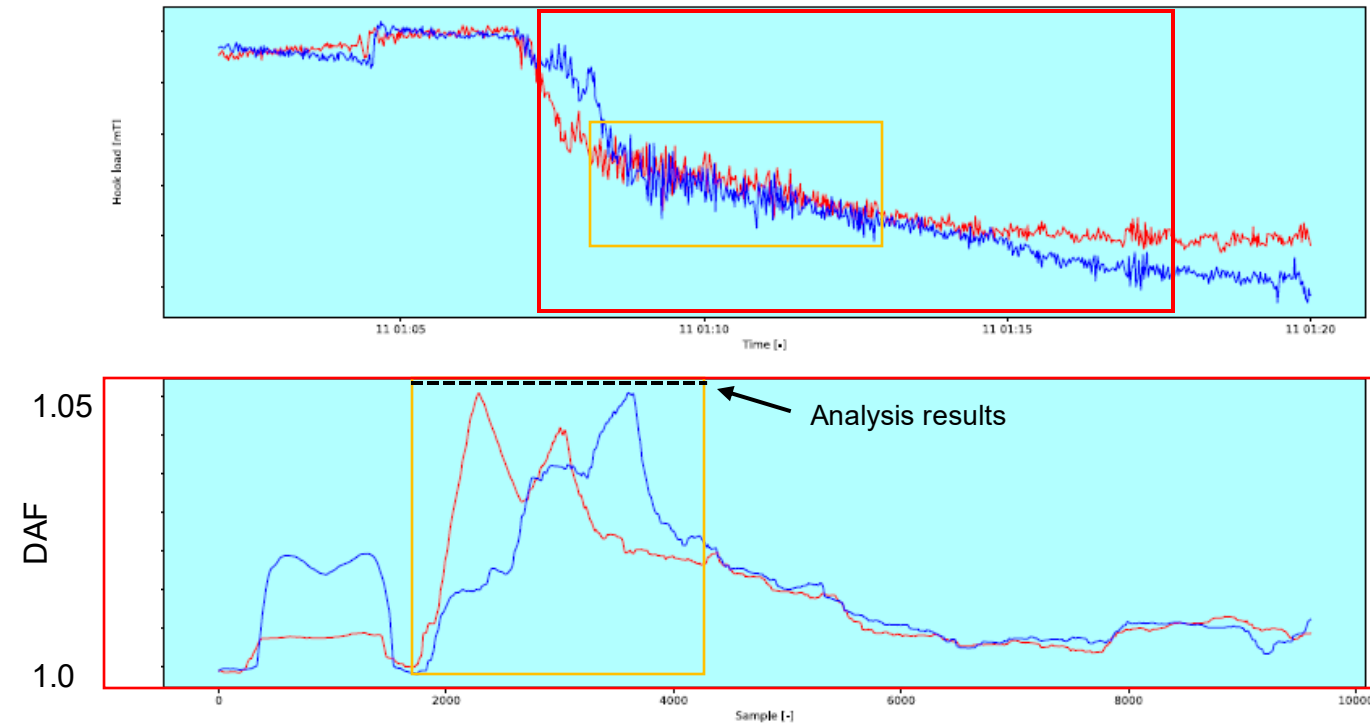
*Jacket lowering
continues*



*Power at higher periods
> 10 s*

Hookload data

- Running average hookload dynamics (2 minute mean)
- Hoistwire dynamics clearly increase
- Hoistwire dynamics are still low
- Good alignment with analysis results



Thank you!

